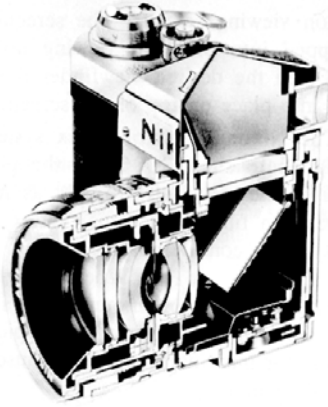


Camera Simulation



Effect	Cause
Field of view	Film size, stops and pupils
Depth of field	Aperture (f-stop), focal length
Motion blur	Shutter
Exposure	Film speed, aperture, shutter

References

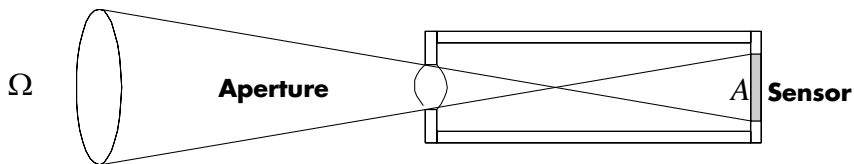
Photography, B. London and J. Upton
 Optics in Photography, R. Kingslake

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Sensor Response

The response of a sensor is proportional to the radiance of the surface visible to the sensor.



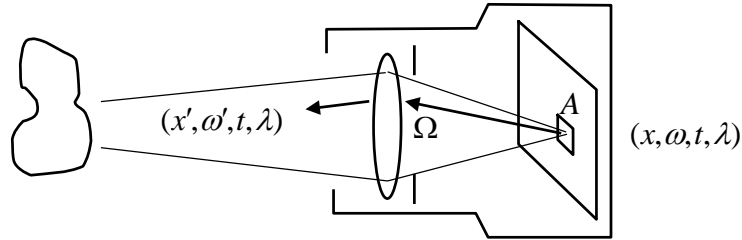
$$R = \int_A \int_{\Omega} L d\omega dA = \bar{L}T$$

$$T = \int_A \int_{\Omega} d\omega dA$$

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The Measurement Equation



$$R = \int \int \int \int_{A \Omega T \Lambda} P(x, \lambda') S(x, \omega, t) L(T(x, \omega, \lambda), t, \lambda) d\vec{A} \bullet d\vec{\omega} dt d\lambda$$

Pixel response	$P(x, \lambda)$
Lens optics	$(x', \omega') = T(x, \omega, \lambda)$
Shutter	$S(x, \omega, t)$
Scene radiance	$L(x, \omega, t, \lambda)$

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Lenses

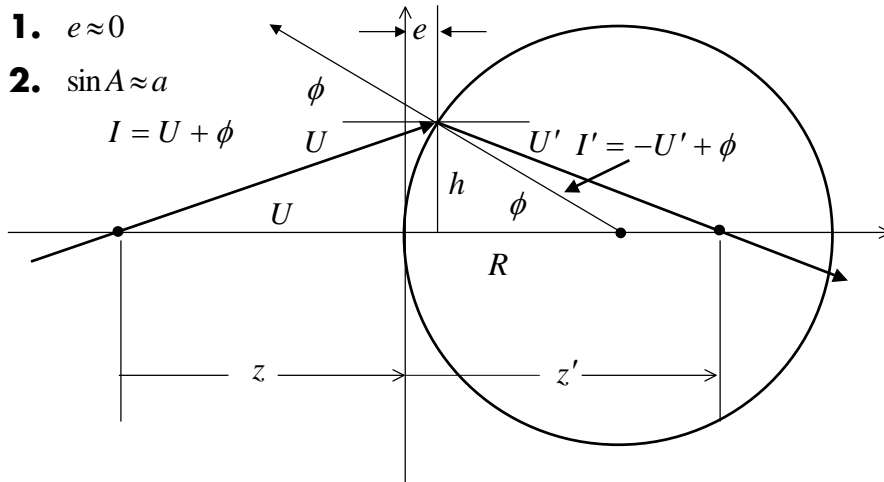
Paraxial Refraction

Paraxial approximation

1. $e \approx 0$

2. $\sin A \approx a$

$$I = U + \phi$$



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Derivation

$$I = U + \phi$$

$$I' = -U' + \phi$$

$$n' \sin I' = n \sin I$$

$$n' i' = n i$$

$$n'(-u' + \phi) = n(u + \phi)$$

$$n' \left(\frac{h}{z'} - \frac{h}{R} \right) = n \left(\frac{h}{z} - \frac{h}{R} \right)$$

$$\frac{n'}{z'} = \frac{n}{z} + \frac{(n' - n)}{R}$$

$$\sin U \approx u \approx \tan U = \frac{h}{z}$$

$$\sin U' \approx u' \approx \tan U' = -\frac{h}{z'}$$

$$\phi = -\frac{h}{R}$$

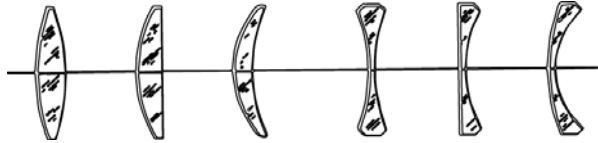
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Lens-makers Formula

Refractive Power

$$P = (n' - n) \left(\frac{1}{R_1} - \frac{1}{R_2} \right) = \frac{1}{f} \quad \left[\frac{1}{m} = \text{diopters} \right]$$

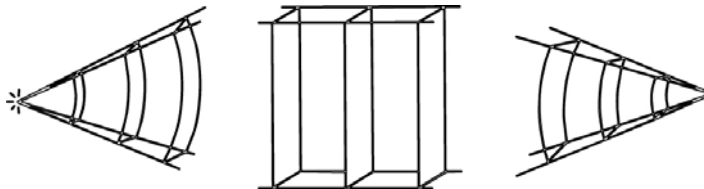


Biconvex Plano-convex

Convex = Converging

Concave = Diverging

Thin Lens Equation



Vergence

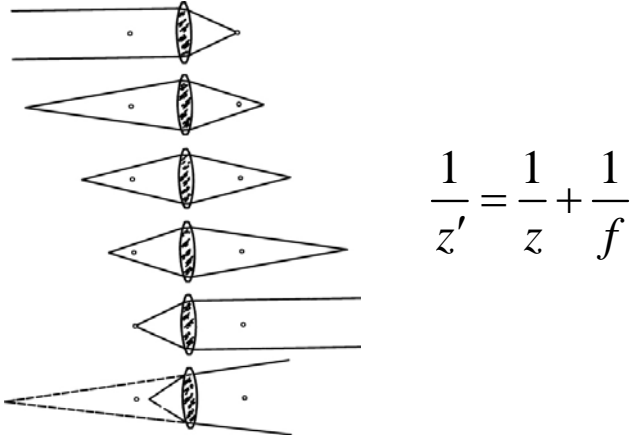
$$V = \frac{n}{r} = \frac{n}{z}$$

Thin lens equation $V' = V + P$

$$\frac{1}{z'} = \frac{1}{z} + \frac{1}{f}$$

Focal Points and Focal Lengths

To focus: move lens relative to backplane



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Perspective Transformation

Thin lens equation

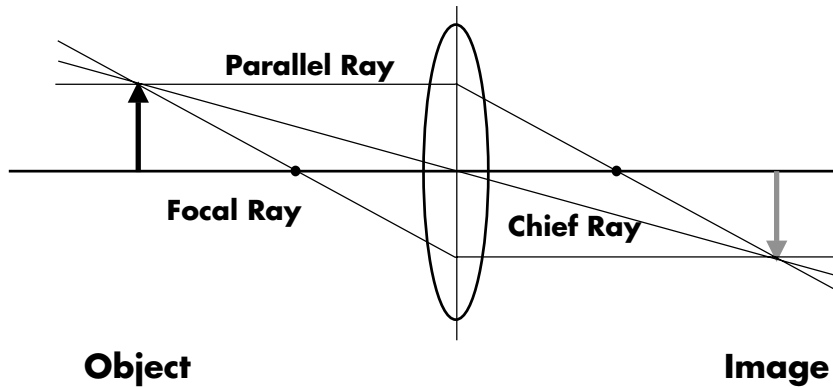
$$\frac{1}{z'} = \frac{1}{z} + \frac{1}{f} \Rightarrow z' = \frac{fz}{z+f}$$
$$\Rightarrow x' = \frac{fx}{z+f}$$

Represent transformation as a 4x4 matrix

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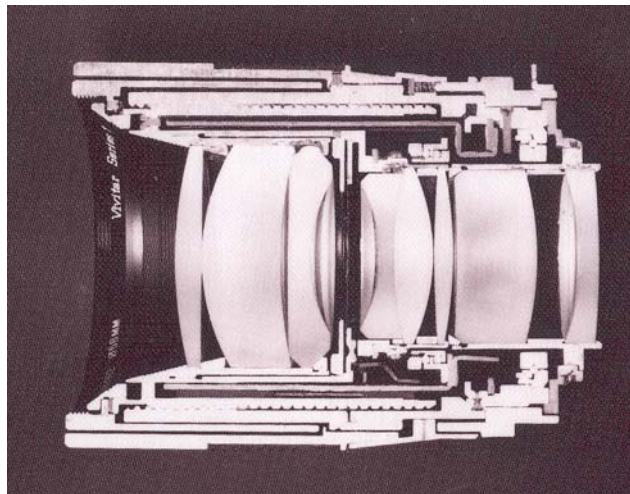
Gauss' Ray Tracing Construction



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Real Lens



Cutaway section of a Vivitar Series 1 90mm f/2.5 lens
Cover photo, Kingslake, *Optics in Photography*

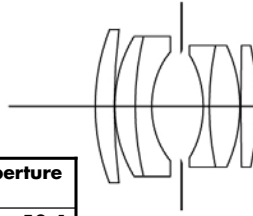
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Double Gauss

Data from W. Smith,
Modern Lens Design, p 312

Radius (mm)	Thick (mm)	n_d	V-no	aperture
58.950	7.520	1.670	47.1	50.4
169.660	0.240			50.4
38.550	8.050	1.670	47.1	46.0
81.540	6.550	1.699	30.1	46.0
25.500	11.410			36.0
	9.000			34.2
-28.990	2.360	1.603	38.0	34.0
81.540	12.130	1.658	57.3	40.0
-40.770	0.380			40.0
874.130	6.440	1.717	48.0	40.0
-79.460	72.228			40.0



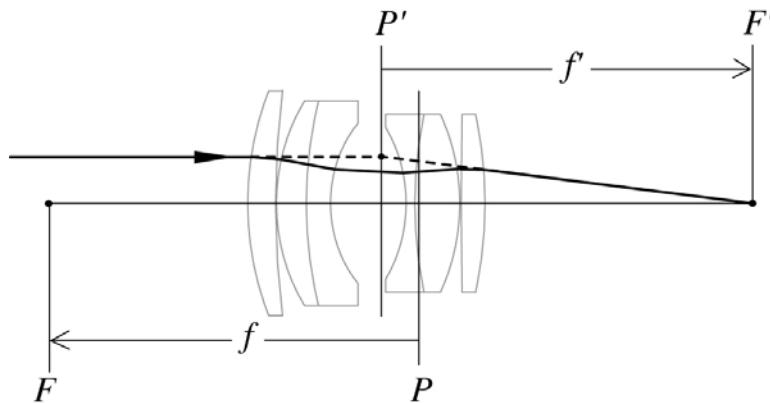
Positive radii = convex

Negative radii = concave

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Thick Lenses



Measure distances from *principal planes*

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Ray Tracing Through Lenses



200 mm telephoto



35 mm wide-angle



50 mm double-gauss



16 mm fisheye

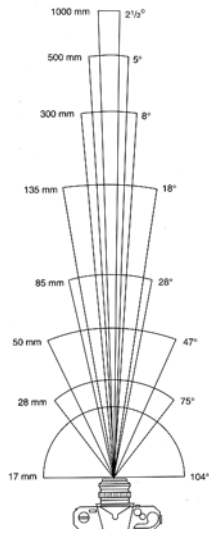
From Kolb, Mitchell and Hanrahan (1995)

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Field of View

Field of View



17mm



28mm



50mm



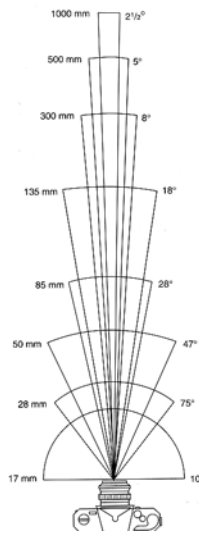
85mm

From London and Upton

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Field of View



135mm



300mm



50mm



From London and Upton

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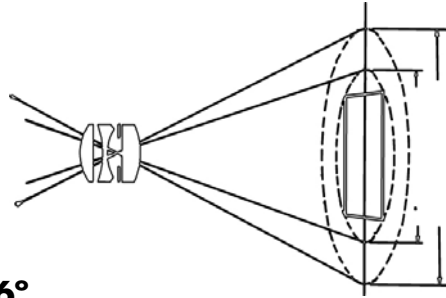
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Field of View

Field of view

$$\tan \frac{fov}{2} = \frac{filmsize}{f}$$

Redrawn from Kingslake,
Optics in Photography



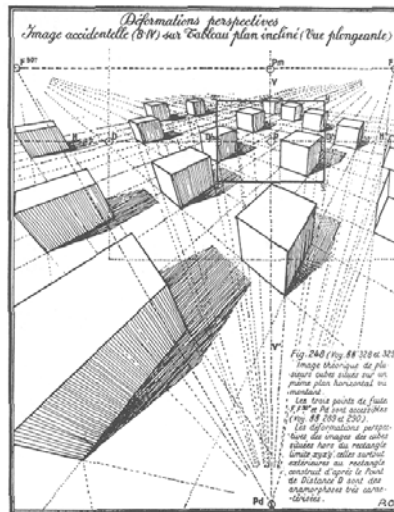
Types of lenses

- Normal 26°
 Film diagonal = focal length
- Wide-angle 75-90°
- Narrow-angle 10°

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Perspective Distortion

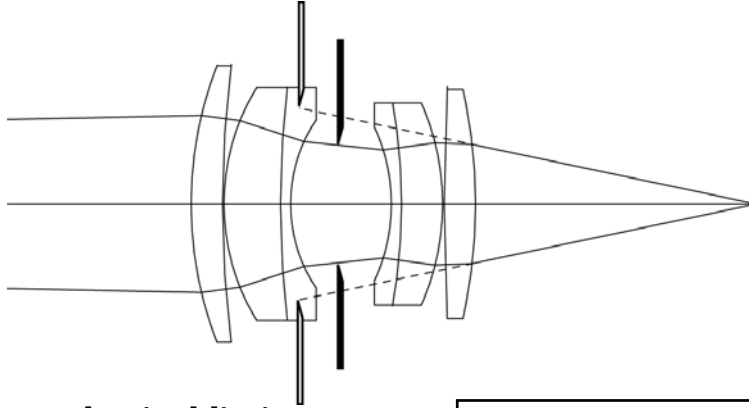


From Olmer, *Perspective Artistique*

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Stops and Pupils



Stops - physical limits
Pupils - logical limits
Exit and entry pupil

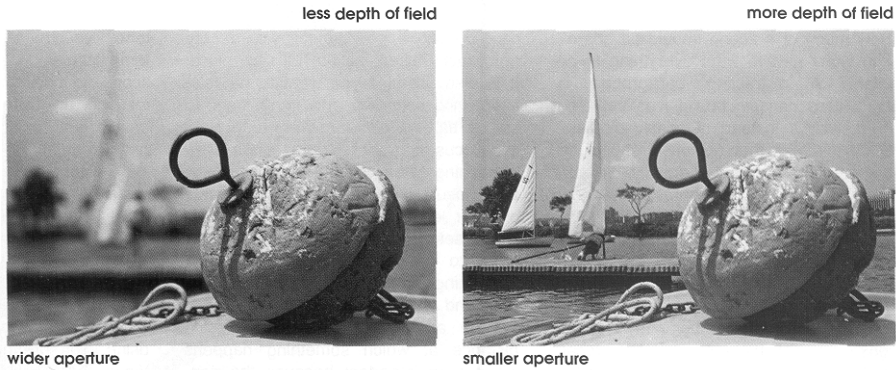
Finite Aperture
1. Depth of field
2. Collects light

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Depth of Field

Depth of Field



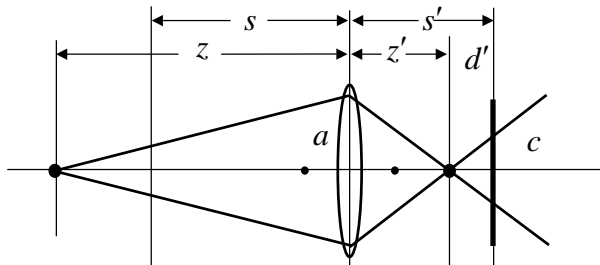
From London and Upton

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Circle of Confusion

Image space view



In-focus

$$\frac{1}{s'} = \frac{1}{s} + \frac{1}{f}$$

Out-of-focus

$$\frac{1}{z'} = \frac{1}{z} + \frac{1}{f}$$

Note: Circle of confusion proportional to the size of the aperture

$$\frac{c}{a} = \frac{d'}{z'} = \frac{s' - z'}{z'}$$

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Depth of Field

Object space view

- Resolving power: sets c

$$\frac{c}{s} = \frac{1}{1000}$$

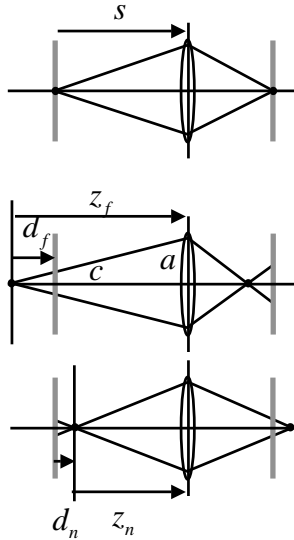
- Depth of field: equal c

$$\frac{c}{a} = \frac{d_f}{z_f} = \frac{d_n}{z_n}$$

- Hyperfocal distance

$$z_n = \frac{2f^2}{c}$$

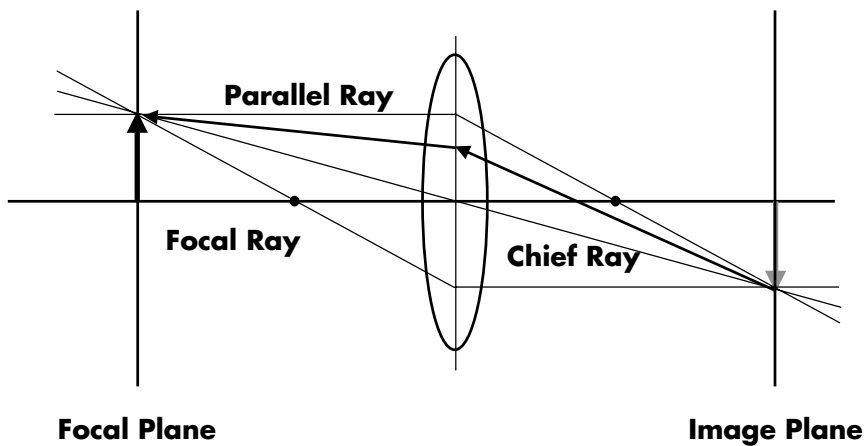
$$z_f = \infty$$



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Ray Tracing: Finite Aperture

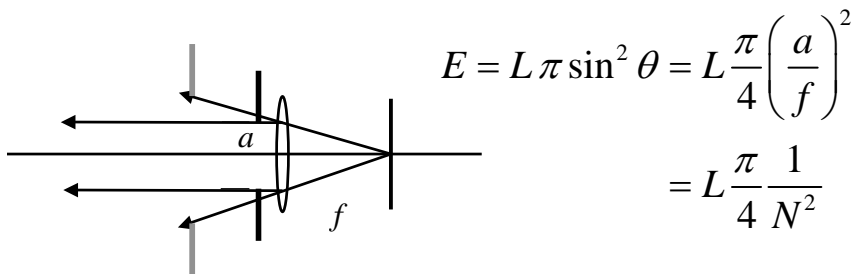


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Exposure

Image Irradiance



F-Stop/F-Number: $a = \frac{f}{N} \Rightarrow N = \frac{f}{a}$

Fstops: 1.4 2 2.8 4.0 5.6 8 11 16 22 32 45 64

1 stop doubles exposure

Camera Exposure

Exposure $H = E \times T$

Exposure overdetermined

Aperture: f-stop - 1 stop doubles H

Interaction with depth of field

Shutter: Doubling the effective time doubles H

Interaction with motion blur

Automatic exposure

Shutter priority

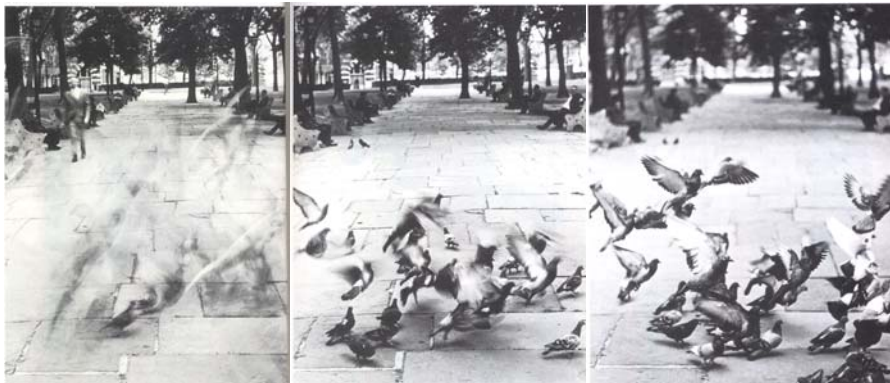
Aperture priority

Programmed

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Aperture vs Shutter



f/16
1/8s

f/4
1/125s

f/2
1/500s

From London and Upton

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Photographic Exposure

Density vs. Transparency

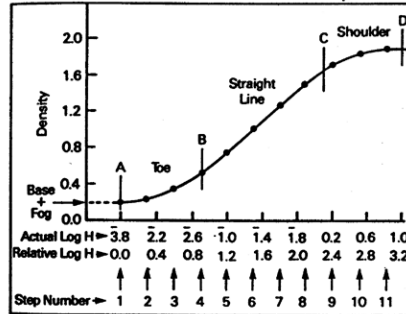
$$D = \log \frac{1}{T}$$

Gamma

$$\gamma = \frac{\Delta D}{\Delta \log H}$$

Film speed

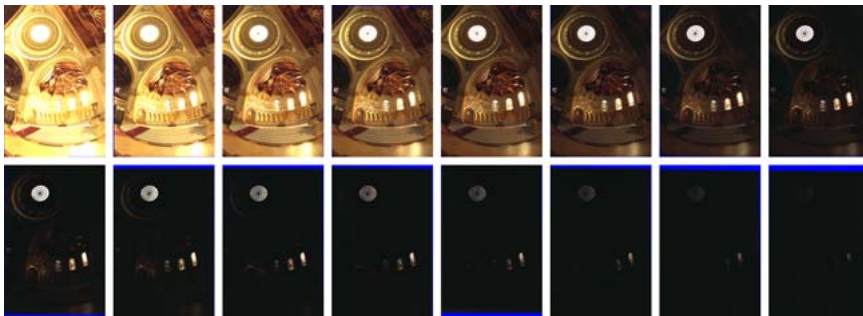
$$Speed = \frac{1}{H} \Rightarrow ISO(ASA) = 0.8 \frac{1}{H_m}$$



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High Dynamic Range



Sixteen photographs of the Stanford Memorial Church taken at 1-stop increments from 30s to 1/1000s.

From Debevec and Malik, High dynamic range photographs.

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Simulated Photograph



Adaptive histogram

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With glare, contrast, blur

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